

## Effects of Annealing and Prior History on Enthalpy Relaxation in Glassy Polymers. 5. Mathematical Modeling of Nonthermal Preaging Perturbations

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**ABSTRACT:** Computer simulation studies of the effects of hydrostatic pressure, tensile stress, and vapor-induced swelling on the physical aging of glass poly(vinyl chloride) (PVC) are presented. Published data indicate that application and rapid release of these nonthermal perturbations before aging produce glasses with elevated enthalpies and increased aging rates compared with those of unstressed glasses. These experimental observations are well described by a modified version of a phenomenological model which gives a good account of purely thermal history effects (Hodge, I. M.; Berens, A. R. *Macromolecules* 1982, 15, 762).

### 1. Introduction

In earlier papers of this series<sup>1-4</sup> it was shown that the effects of physical aging on enthalpy relaxation in polymers are described with good accuracy by a four-parameter phenomenological model based on the work of Tool,<sup>5</sup> Narayanaswamy,<sup>6</sup> Mazurin et al.,<sup>7</sup> and DeBolt et al.<sup>8</sup> This model reproduces the effects of cooling rate, aging time, aging temperature, and heating rate on the temperature and magnitude of heat capacity maxima observed in many aged polymers<sup>2</sup> and can be fitted to experimental data by standard optimization procedures.<sup>3,4</sup> In this paper we extend the model to include the effects on physical aging of hydrostatic pressure, tensile stress, and vapor-induced swelling, applied and released before aging. Our goal is to reproduce, qualitatively, experimental data with a calculation procedure which is computationally efficient and convenient.

We first review published experimental data that are relevant to our modeling studies. The effects of hydrostatic pressure on enthalpy relaxation in polymers have been studied experimentally by several investigators. Weitz and Wunderlich<sup>9</sup> observed isobaric heat capacity maxima in DSC scans, at 5 K min<sup>-1</sup> and atmospheric pressure, of polystyrene (PS) and poly(methyl methacrylate) (PMMA) glasses formed by cooling at 5 K h<sup>-1</sup> under hydrostatic pressures ranging from 0 to 345 MPa (0–3.45 kbar). At low pressure (69 MPa) the large heat capacity overshoot near  $T_g$ , characteristic of slowly cooled and rapidly heated glasses, was diminished compared with that of the glass formed at atmospheric pressure. At intermediate pressure (207 MPa) the heat capacity maximum moved to a lower temperature,  $T_{max}$ , to appear as a sub- $T_g$  peak (magnitude  $C_{p,max}$ ), similar to those observed by Illers<sup>10</sup> and others<sup>1,11-13</sup> in aged PVC glasses formed at atmospheric pressure. At the highest pressure (345 MPa) a broad exothermic heat capacity minimum developed between  $T_{max}$  and  $T_g$ . Similar results were observed by Yourtee and Cooper,<sup>14</sup> Dale and Rogers,<sup>15</sup> and Wetton and co-workers<sup>16,17</sup> for PS and by Kimmel and Uhlmann<sup>18</sup> and Price<sup>19</sup> for PMMA. For nonpolymeric glasses [phenolphthalein, sucrose, KNO<sub>3</sub>/

Ca(NO<sub>3</sub>)<sub>2</sub>] Weitz and Wunderlich observed only a decrease in overshoot near  $T_g$  with increasing pressure.<sup>9</sup> Prest and co-workers<sup>12,13</sup> reported heat capacity data obtained during heating at 20 K min<sup>-1</sup> for PVC formed by cooling at 20 K min<sup>-1</sup> under hydrostatic pressures ranging from 100 to 600 MPa and aged at room temperature and atmospheric pressure for 110 days. The sub- $T_g$  heat capacity peak moved to slightly lower temperatures and became more asymmetric with increasing pressure. Berens and Hodge<sup>1,11</sup> observed that cold drawing, powder compaction, and vapor-induced swelling of glassy PVC accelerated the rate of sub- $T_g$  peak development with aging time but noted that  $T_{max}$  was a weak function of the type and magnitude of the nonthermal perturbation. Similar findings were reported by Shultz and Young<sup>20</sup> for freeze-dried PS and PMMA and by Prest and Roberts<sup>12</sup> for mechanically compacted PS powder.

### 2. Modeling Studies

Before describing the introduction of nonthermal perturbations, we first review the model and calculation procedure described in detail elsewhere<sup>2</sup> for purely thermal histories.

**2.1. Thermal Histories.** The calculation procedure treats cooling and heating as a series of temperature steps and isothermal holds whose relative magnitudes are determined by the cooling and heating rates. Aging is introduced as an isothermal hold during cooling. The response of enthalpy to each temperature step is described by a response function  $\phi(t)$ , which for convenience and good accuracy is chosen to be of the form

$$\phi(t) = \exp[-(t/\tau_0)^\beta] \quad (1)$$

The ratio  $t/\tau_0$  is the reduced time

$$t_r = t/\tau_0 \quad (2)$$

The relaxation time  $\tau_0$  depends on temperature  $T$  and fictive temperature  $T_f$  according to the empirical Narayanaswamy expression<sup>6</sup>

$$\tau_0 = A \exp \left[ \frac{x\Delta h^*}{RT} + \frac{(1-x)\Delta h^*}{RT_f} \right] \quad (3)$$

where  $x$  is a numerical measure of nonlinearity ( $1 \geq x >$

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0),  $\Delta h^*$  is an activation enthalpy that determines the cooling rate dependence of  $T_g$ ,<sup>21</sup> and  $A$  and  $\Delta h^*$  together determine  $T_g$ :

$$\ln A \approx \ln \tau_0|_{T=T_g} - \Delta h^*/RT_g \quad (4)$$

By continually updating  $\tau_0$  as  $T_f$  relaxes in response to each temperature step, the nonlinearity is removed and the response to cooling, aging, and heating can be calculated by applying Boltzmann superposition. It is assumed that  $A$ ,  $\beta$ ,  $x$ , and  $\Delta h^*$  are independent of  $T$  and  $T_f$ .

The calculated heat capacity,  $dT_f/dT$ , corresponds to the experimental normalized heat capacity  $C_p^N$ , which has values of 0 and 1 in the glassy and liquid state, respectively.

**2.2. Nonthermal Preaging Perturbations.** **2.2.1. Hydrostatic Pressure.** Pressure increases  $T_g$  and is introduced into the model by lengthening  $\tau_0$  in eqs 1 and 3. This can be accomplished in three ways, all of which produce similar results: either  $\Delta h^*$  or  $A$  can be increased or  $T_f$  decreased such that  $T_f < T$  at equilibrium for  $P > 0$ . For the experimental protocols considered here changes in  $\Delta h^*$ ,  $A$ , or  $T_f$  are applied during cooling from above  $T_g$  to the aging temperature and removed during aging and reheating. The magnitude of these changes as a function of pressure can be estimated, with sufficient accuracy for our qualitative purposes, from the enthalpy-based Ehrenfest relation

$$(\partial T/\partial P)_H = -T_g V_g \Delta \alpha / \Delta C_p \quad (5)$$

where  $\Delta \alpha$  and  $\Delta C_p$  are the changes in thermal expansivity and isobaric heat capacity and  $V_g$  is the volume at the glass transition temperature  $T_g$ . This relation has been shown to be reasonably accurate for polymers.<sup>22</sup> The constancy of  $H$  for the partial derivative in eq 5 corresponds to fixed enthalpic fictive temperature, and differentiation of eq 3 at constant  $T_f$  gives for  $T \approx T_f \approx T_g$

$$d \ln \tau_0|_{T_f}^P = \frac{-x \Delta h^*}{RT^2} dT \approx \frac{x \Delta h^*}{RT_g} \frac{V_g \Delta \alpha}{\Delta C_p} dP \quad (6)$$

The corresponding changes in  $\Delta h^*$ ,  $T_f$ , and  $A$  required to change  $\ln \tau_0$  by this amount are

$$d(\Delta h^*)^P \approx \frac{x \Delta h^* V_g \Delta \alpha}{\Delta C_p} dP \quad (7)$$

$$dT_f^P \approx \left( \frac{-x}{1-x} \right) \frac{T_g V_g \Delta \alpha}{\Delta C_p} dP \quad (8)$$

$$d(\ln A)^P \approx \frac{x \Delta h^*}{RT_g} \frac{V_g \Delta \alpha}{\Delta C_p} dP \quad (9)$$

For  $T \approx T_e < T_g$ , where  $T_e$  is the aging temperature, the right-hand sides of eq 7-9 are multiplied by a factor of order  $(T_g/T_e)^2$ . It is assumed for simplicity that  $x$  and  $\beta$  are independent of pressure and that  $d(\Delta h^*)^P$ ,  $dT_f^P$ , and  $d(\ln A)^P$  are the same in both liquid and glassy states (i.e.,  $T_g/T_e \approx 1$ ).

In some cases the original procedure<sup>2</sup> of dividing the aging time into 10 logarithmically even intervals produced initial time increments that were too long compared with the relaxation time and gave changes in  $T_f$  that lay outside the linear range ( $>2$  K). To avert this the aging time (in seconds) was divided into 10 logarithmically even divisions per decade. With this procedure changes in  $T_f$  never exceeded 2 K per time step, and the computation time did not increase excessively.

**2.2.2. Vapor-Induced Swelling and Mechanical Stress.** The increased volume and configurational entropy

of vapor-swollen PVC are expected to shorten the average relaxation time, in qualitative accord with the well-known WLF and Adam-Gibbs expressions. For cold-drawn PVC film, dilation is expected to occur as a result of a Poisson ratio less than 0.5, again resulting in a shortened relaxation time (as discussed by Matsuoka<sup>23</sup>). Both perturbations can therefore be introduced into the calculation as a decrease in  $\tau_0$  immediately before aging. As in the calculation of hydrostatic pressure effects, the change in  $\tau_0$  can be effected by variation of  $\Delta h^*$ ,  $A$ , or  $T_f$  with similar results. The calculation results presented here were obtained by varying  $T_f$  by an amount  $\Delta T_f^s$ . The changes in  $\tau_0$  are assumed to occur instantaneously at the start of aging, this being justified by the rapid removal of stress and swelling perturbations (in seconds) compared with the aging times (a minimum of 1 h).<sup>1,11</sup> The change in  $\tau_0$  decays with reduced time during aging and reheating according to eq 1 and 2. For the case of  $\Delta T_f^s$

$$\Delta T_f^s(t_r) = \Delta T_f^s \exp[-(t_r - t_0)^\beta] \quad (10)$$

where  $\Delta T_f^s$  is the instantaneous change in  $T_f$  before aging and  $t_0$  is the elapsed reduced time at the start of aging. The response described by eq 10 is superimposed on the response to the thermal history, the two being coupled by their common dependence of  $\tau_0$  on  $T_f$  and  $T$ . The procedure is illustrated schematically in the inset of Figure 5.

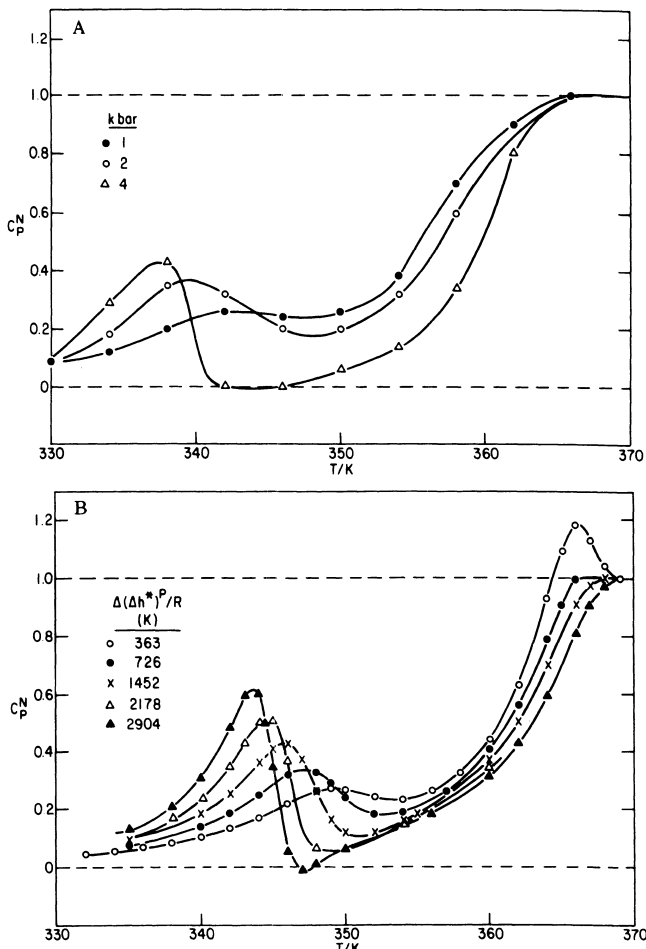
The numerical changes in relaxation time induced by tensile stress and swelling are not as readily estimated as they are for hydrostatic pressure. Accordingly, values of  $\Delta T_f^s$  in eq 10 were obtained empirically by matching the calculated and experimental values of  $C_{p,\max}^N$  for a fixed aging time (24 h in the present study), and the accuracy of the model is assessed by comparing the experimental and calculated values of  $C_{p,\max}^N$  and  $T_{\max}$  at other aging times.

### 3. Results

**3.1. Experimental Data.** **3.1.1. Hydrostatic Pressure.** Experimental heat capacity data for PVC obtained by Prest and Roberts<sup>12</sup> for three pressures are shown in Figure 1A in normalized form. Their highest pressure data are omitted since they were obtained on a sample that vitrified during pressurization before cooling.

**3.1.2. Vapor-Induced Swelling and Tensile Stress.** Experimental data of Berens and Hodge<sup>11</sup> on the effects of preaging exposure to varied pressures of CO<sub>2</sub> and CH<sub>3</sub>Cl vapor on the DSC curves of aged PVC powder are shown in Figures 2 and 3. The particular pressures were chosen, by reference to independently determined sorption isotherms, to give approximately equal weight percent sorption of the two vapors: Curves A, B, C, and D in Figures 2 and 3 correspond to about 0, 1, 2, and 4 wt % sorption, respectively, of CO<sub>2</sub> and CH<sub>3</sub>Cl (since CH<sub>3</sub>Cl is more soluble, lower pressures were required to reach equal sorption). With both vapors, there is a progressive increase in the height of the DSC aging peak, and a small shift to lower  $T_{\max}$ , with increasing vapor pressure. The similarity of the two sets of curves clearly suggests that aging is affected by the extent of sorption or dilation of the polymer, and not by the vapor pressure per se. A summary of the experimental values of  $C_{p,\max}^N$  and  $T_{\max}$  as a function of vapor pressure is given in Table I.

DSC curves for PVC sheet samples aged after application and release of tensile stresses, also obtained by Berens and Hodge,<sup>11</sup> are shown in Figure 4. Preaging tensile stress up to 75% of the yield stress produced little effect on enthalpy relaxation (curves A and B), but stressing to and beyond the yield point (curves C and D) caused a



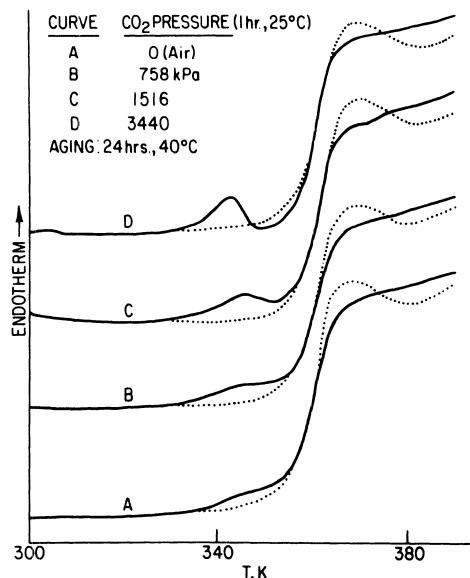
**Figure 1.** (A) Normalized experimental heat capacities of PVC, after cooling at  $20 \text{ K min}^{-1}$  at the indicated hydrostatic pressures and aging at room temperature and pressure for 110 days. Heating rate  $20 \text{ K min}^{-1}$  at atmospheric pressure. Raw heat capacity data from Prest and Roberts.<sup>12</sup> (B) Calculated normalized heat capacities of PVC for the indicated values of  $\Delta(\Delta h^*)^P$  (see section 2.2.1 of text) and the same thermal history as in (A). Unperturbed parameters were  $\ln A$  (s) =  $-619.0$ ,  $\Delta h^*/R = 225 \times 10^3 \text{ K}$ ,  $x = 0.11$ , and  $\beta = 0.25$ .

**Table I**  
Observed and Calculated Effects of Preaging Perturbations  
(after Aging 24 h at 313 K)

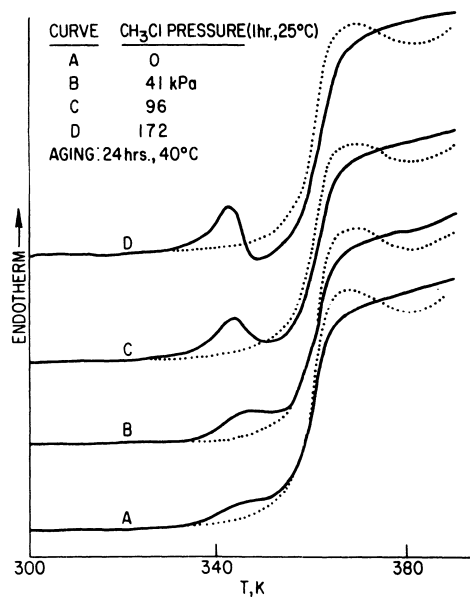
exptl perturbation	$\Delta T_f^s$	$T_{\max}$ , K		$C_{p,\max}^N$	
		exptl ( $\pm 1$ K)	calcd ( $\pm 1$ K)	exptl ( $\pm 0.02$ )	calcd ( $\pm 0.01$ )
$P_{\text{CO}_2}$ , MPa					
0	0	347 (sh) <sup>a</sup>	346	0.16	0.18
0.76	0	346	346	0.15	0.18
1.52	1	345	344	0.20	0.21
3.44	2	343	343	0.22	0.24
$P_{\text{CH}_3\text{Cl}}$ , MPa					
0	0	347 (sh)	346	0.16	0.18
0.041	0.5	346	345	0.19	0.19
0.096	1	344	344	0.22	0.21
0.172	2	343	343	0.24	0.24
tensile stress, MPa					
0	0	347 (sh)	346	0.16	0.18
46	3	340	342	0.23 ( $\pm 0.04$ )	0.28

<sup>a</sup>Shoulder.

pronounced DSC aging peak. Curve D for the material stressed beyond the yield point also exhibits a strong exotherm and shift in  $T_g$ . These are thought to be due to release of energy stored as orientation.<sup>11</sup> Values of  $C_{p,\max}^N$  and  $T_{\max}$  corresponding to curve C in Figure 4 are also



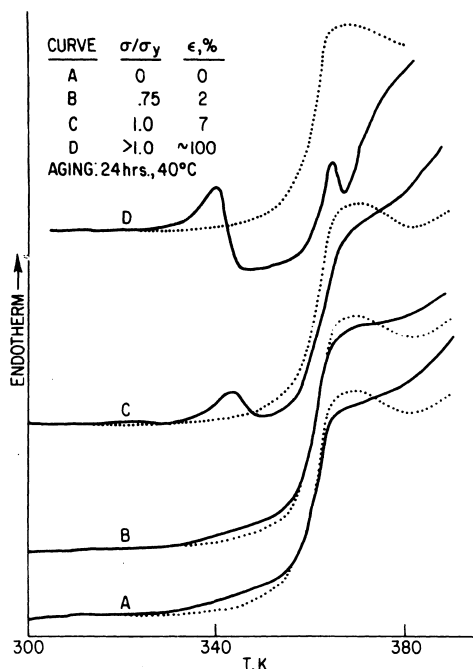
**Figure 2.** DSC curves for free-cooled PVC powder, after preaging exposure to  $\text{CO}_2$  at the indicated vapor pressure for 1 h at  $25^\circ\text{C}$ , and after aging for 24 h at  $40^\circ\text{C}$ .<sup>11</sup>



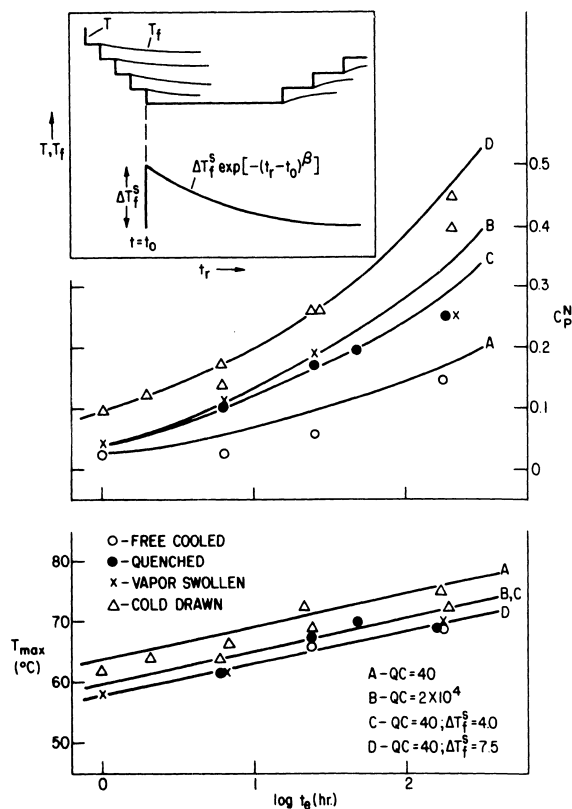
**Figure 3.** DSC curves for free-cooled PVC powder, after preaging exposure to  $\text{CH}_3\text{Cl}$  at the indicated vapor pressures for 1 h at  $25^\circ\text{C}$ , and after aging for 24 h at  $40^\circ\text{C}$ .<sup>11</sup>

included in Table I. A summary of earlier experimental results obtained by Berens and Hodge for PVC<sup>1</sup> are reproduced in Figure 5 in the form of  $C_{p,\max}^N$  and  $T_{\max}$  vs. aging time, for the indicated thermal and nonthermal preaging histories. In these studies the tensile stress history of the films<sup>1,11</sup> consisted of cold drawing to just above the yield point (about 100% elongation) in an Instron, followed by stress removal immediately before aging at  $40^\circ\text{C}$ .

**3.2. Calculation Results. 3.2.1. Preaging Hydrostatic Pressure.** Insertion of the experimental values of  $\Delta C_p$ ,  $\Delta\alpha$ ,  $V_g$ , and  $T_g$  for PVC into eq 7-9 [ $\Delta C_p = 0.10 \text{ K}^{-1} \text{ g}^{-1}$ ,<sup>24</sup>  $\Delta\alpha \approx 2 \times 10^{-4} \text{ K}^{-1}$ ,<sup>22</sup>  $V_g = 0.7 \text{ cm}^3 \text{ g}^{-1}$ ,  $T_g = 363 \text{ K}$ ,<sup>2</sup>  $x = 0.11$ ,<sup>2</sup>  $\Delta h^*/R = 225 \times 10^3 \text{ K}^2$ ] gives  $\Delta(\Delta h^*)^P/R\Delta P \approx 8.4 \text{ K MPa}^{-1}$ ,  $\Delta T_f^P/\Delta P \approx 0.015 \text{ K MPa}^{-1}$  and  $\Delta(\ln A)^P/\Delta P \approx 0.023 \text{ MPa}^{-1}$ . Calculated values of  $C_{p,\max}^N$  and  $T_{\max}$  for equivalent changes in  $T_f$ ,  $\Delta h^*$ , and  $\ln A$  for PVC are listed in Table II. Almost identical results are obtained for each calculation procedure. Calculated nor-



**Figure 4.** DSC curves for free-cooled PVC film, after preaging tensile stresses were applied for 10 min (curves A, B, and C), and after aging 24 h at 40 °C. Yield stress ( $\sigma_y$ ) is about 46 MPa. Curve D is for film cold drawn to 100% elongation at 1% min<sup>-1</sup>.<sup>11</sup>



**Figure 5.** Experimental data points<sup>1</sup> and calculated curves for the aging time dependences of  $C_{p,max}^N$  and  $T_{max}$  for PVC for the indicated thermal and nonthermal histories. Inset: Schematic of the calculation procedure (see section 2.2.2 of text).

malized heat capacities, using atmospheric pressure parameters for PVC obtained from purely thermal histories,<sup>2</sup> are shown in Figure 1B for the indicated values of  $\Delta(\Delta h^*)^P$ . The experimentally observed sharpening and increased asymmetry of the sub- $T_g$  heat capacity peaks with pressure, the modest decrease in  $T_{max}$ , and the increase in  $T_g$  are all reproduced by the calculation.

**Table II**  
Calculated  $C_{p,max}$  and  $T_{max}$  for Parameter Increments  $Q_C = 20 \text{ K min}^{-1}$ ,  $Q_H = 20 \text{ K min}^{-1}$ ,  $t_e = 24 \text{ h}$ , and  $T_e = 313 \text{ K}$

hydrostatic pressure, MPa	parameter increments	$C_{p,max}$	$T_{max}, \text{K}$	
0	$-\Delta T_f^P \text{ (K)}$	0	0.167	347
100		1.52	0.205	344
200		3.04	0.251	342
400		6.08	0.350	340
600		9.12	0.460	339
0	$\Delta \ln A$	0	0.167	347
100		2.32	0.205	344
200		4.65	0.251	342
400		9.30	0.353	340
600		13.94	0.465	339
0	$\Delta(\Delta h^*/R) \text{ (K)}$	0	0.167	347
100		844	0.205	344
200		1689	0.249	342
400		3377	0.346	340
600		5066	0.455	339

**3.2.2. Preaging Tensile Stress and Vapor-Induced Swelling.** The calculated dependences of  $C_{p,max}^N$  and  $T_{max}$  on aging time, using  $\Delta T_f^s$  to change  $\ln \tau_0$ , are shown as solid lines in Figure 5. As stated in section 2.2.2 the value of  $\Delta T_f^s$  for the perturbed glasses was determined from  $C_{p,max}^N$  for an aging time of 24 h. For the unperturbed glasses no adjustable parameter was introduced, and the deviations between experimental and calculated curves in this case are due in part to the relatively large experimental uncertainties in  $C_{p,max}^N$  and  $T_{max}$  for small sub- $T_g$  peaks and to uncertainty in the (uncontrolled) cooling rate. The unperturbed parameters for PVC were those used in the hydrostatic pressure calculations, i.e., those obtained from analysis of purely thermal histories.<sup>2</sup> The calculated values of  $T_{max}$  and  $C_{p,max}^N$  as a function of  $\Delta T_f^s$  are compared with experimental values in Table I. There is excellent agreement between the calculated and experimentally observed relations between  $T_{max}$  and  $C_{p,max}^N$ .

#### 4. Discussion

The ability of the mathematical model to reproduce the effects of hydrostatic pressure, vapor-induced swelling, and tensile stress, as well as thermal history, on subsequent enthalpy relaxation in PVC supports our previous suggestion<sup>11</sup> that the nonthermal preaging treatments may all be regarded as a generalized stress whose release increases the enthalpy of the glass. This results in the glass being further from equilibrium at the start of aging, and thus losing enthalpy more rapidly than an unstressed material.

The overall agreement between calculated and experimental results for the effects of hydrostatic pressure, tensile stress, and vapor-induced swelling on the physical aging of PVC indicates that the calculation procedures are essentially correct. In particular, the assumption that these nonthermal perturbations change only the relaxation time appears to be valid. Any changes in the shape parameter  $\beta$  with  $T$  or  $T_f$  are evidently of minor importance, but it is not clear from the present results whether this is due to the changes being numerically very small or if the calculated results are simply insensitive to them (variation of  $\beta$  with  $T$  or  $T_f$  would require a different calculation procedure and was not attempted). Recently published theoretical results,<sup>25-28</sup> which predict that small changes in  $\beta$  with  $T_f$  produce large changes in  $\tau_0$ , suggest the former is more likely; evidently the effects of nonlinearity are much more important than those of changing  $\beta$ .

The experimental data shown in Figure 5 indicate that  $T_{max}$  increases approximately linearly with  $\log t_e$ , with a slope (about 5 K decade<sup>-1</sup>) that is independent of history.

The calculated results reproduce these features. The calculated negative dependence of  $T_{\max}$  on  $\Delta T_f^s$  is comparable with the experimental scatter in these early results<sup>1</sup> but is confirmed by the more recent experimental results<sup>11</sup> shown in Table I: increases in vapor pressure of both  $\text{CO}_2$  and  $\text{CH}_3\text{Cl}$ , which swell PVC to increasing extents and which would be expected to correspond to increasing values of  $\Delta T_f^s$ , decrease  $T_{\max}$  slightly. Additional confirmation of the calculated small negative value of  $dT_{\max}/d\Delta T_f^s$  is provided by the small shifts to lower  $T_{\max}$  of the sub- $T_g$  peaks observed for increasing cold-drawing elongations of PVC film.<sup>11</sup> Increasing levels of cold compaction of PVC powder also produce increases in  $C_{p,\max}^N$  and small decreases in  $T_{\max}$ .<sup>11</sup> In the last case localized intergranular stresses are thought to exceed the yield stress, resulting in cold flow and a deformation mode similar to that obtained by cold drawing.

The insensitivity of  $T_{\max}$  to the magnitude of nonthermal perturbations enables a test to be made of the prediction<sup>2</sup> that  $T_{\max}$  is a strong function of  $T_e$  but a relatively weak function of  $T_g - T_e$ , at fixed  $t_e$ . Prest and Roberts<sup>12</sup> observed sub- $T_g$  peaks in mechanically perturbed blends of narrow molecular weight distribution polystyrenes, whose  $T_g$  values ranged from ca. 330 to ca. 375 K. They found that  $T_{\max}$ , for  $T_e \approx 300$  K and  $t_e = 5$  days, varied from about 335 K for the low- $T_g$  component to 345 K for the high- $T_g$  component. This range is much smaller than the variation in  $T_g$ . Because of the small effect of mechanical stresses on  $T_{\max}$ , a similarly small variation in  $T_{\max}$  would also be expected for unperturbed aged glasses of varying  $T_g$  but similar chemical nature. The calculated result<sup>2</sup> is consistent with this expectation.

The closely similar behavior of rapidly quenched and vapor-preswollen PVC glasses, noted earlier<sup>1,2</sup> and evident in Figure 5, is in apparent conflict with the memory effect associated with nonexponential decay functions. It might be expected that glasses with elevated enthalpies formed by slow cooling and vapor-induced swelling might age differently from glasses formed by rapid quenching. However, the memory effect occurs only when the reduced times taken to reach a particular state by different paths are comparable with the subsequent reduced evolution time, whereas (as noted above) the elevated enthalpies of both vapor-treated and rapidly quenched PVC glasses are acquired very rapidly compared with the aging times.

Turning now to hydrostatic pressure, we note that although only qualitative reproduction of experimental trends was aimed for in these calculations the agreement between experimental and calculated results for PVC is quantitatively quite good. In particular, the changes in magnitude and shape of the sub- $T_g$  peaks and their shift with pressure are reproduced with good accuracy. The small shift in  $T_g$  is also calculated correctly. The values of  $\Delta(\Delta h^*)$  which best reproduce the experimental data are about half those calculated from eq 7. This discrepancy could be due to experimental uncertainties in  $\Delta\alpha$  and  $\Delta C_p$ , differences in the PVC's used by Prest and Roberts<sup>12</sup> and Berens and Hodge,<sup>1</sup> or inadequacy of eq 5. In any event, agreement within a factor of 2 for the values of  $\Delta(\Delta h^*)$  is

considered good enough to be regarded as support for the essential correctness of the calculation procedure.

Finally, we observe that the effects on physical aging of PVC induced by hydrostatic pressure, applied during cooling to the glassy state and then released, are similar to those induced by increased quench rate, tensile stress, and vapor-induced swelling. This is surprising at first glance since rapid quench rates and the stress and swelling perturbations produce higher initial fictive temperatures and shorter relaxation times whereas pressurized glasses have longer relaxation times. However, pressure release before aging produces glasses which, although densified, have higher enthalpy and shorter enthalpic relaxation times than glasses formed by cooling at the same rate at zero pressure. This phenomenon is well recognized<sup>9,22</sup> and its reproduction by the calculation procedure described here is further evidence of the essential correctness of the model.

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